

1 **FOAM, a new simple benthic degradative**
2 **module for the LAMP3D model: an**
3 **application to a Mediterranean fish farm**

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20 **Abstract**

21

22 The modeling framework already introduced by Doglioli et al. (2004a) to predict
23 the potential impact of a marine fish farm is improved following different directions.
24 Namely: (i) real historic current-meter data are used to force the simulations; (ii)
25 settling velocity values specifically targeting Mediterranean fish species are used; and
26 (iii) a new benthic degradative module, FOAM, is added to the modeling framework.
27 FOAM uses the output of the other functional units of the modeling framework to
28 calculate the organic load on the seabed. FOAM considers the natural capability of
29 the seafloor in absorbing part of the organic load. Different remineralization rates
30 reflect the sediment stress level according to the work of Findlay & Watling (1997).

31 Organic degradation for both uneaten feed and faeces is evaluated by changing
32 release modality (continuous and periodical) and by varying the settling velocities.
33 It is found that the maximum impact on the benthic community is observed either
34 for quickly-sinking uneaten feed released twice a day, or for less intense near bottom
35 current conditions. If both the above mentioned scenarios coexist, a high stress level
36 is established in the sediment. The model also suggests that the use of self-feeders
37 in cages can significantly reduce farm impacts. These results show how the new and
38 more complete modeling framework presented here is able to improve the objectivity
39 in the decision making processes and how it may be successfully used for planning
40 and monitoring purposes.

1 Introduction

The increase in global fish consumption and the decrease of wild fish stocks are the main reasons behind the continuous development of marine aquaculture (FAO Fisheries Division, 2006, <http://www.fao.org/docrep/009/a0874e/a0874e00.htm>).

The worldwide expansion of marine fish farms, however, has always been generating concern regarding the possible impacts on coastal ecosystems. Already in 1995, the Food and Agriculture Organization (FAO) of the United Nations adopted a Code of Conduct for Responsible Fisheries. The Code provided the necessary framework for national and international efforts to ensure sustainable exploitation of aquatic living resources. Particular attention was paid to the aquaculture growth in accord with the sustainable and integrated use of the environment, taking into account the fragility of coastal ecosystems, the finite nature of their natural resources and the needs of coastal communities. In 2001, following the same direction, the European Union started to set up a strategy for sustainable aquaculture development with the Biodiversity Action Plan for Fisheries (COM 162, 2001) and the European Strategy for Sustainable Development (COM 264, 2001). These two documents led to the more recent and specific Strategy for the Sustainable Development of European Aquaculture (COM 511, 2002).

Marine aquaculture operations are still very expensive, and the only means by which profitability can be sustained is to intensify fish production. Unfortunately this intensification increases the already existing concerns about reaching and surpassing the natural capability of the environment. The scientific literature has identified the main environmental impact from fish farms to be the release of particulate waste products (Hall et al., 1990; Holmer & Kristensen, 1992; Karakassis et al., 2000). The particulate wastes increase the organic load on the benthic environment and might determine changes in the community structure and in the biodiversity of the benthic assemblages (Tsutsumi et al., 1991; Wu et al., 1994; Vezzulli et al., 2002, 2003). Therefore we are in need for predictive tools able to assess whether or

69 not the establishment of a new farm (or the permission for an increase in produc-
70 tion of an already existing one), can result in a potential impact on the surrounding
71 environment.

72 Numerical models can be used to perform environmental impact predictions and
73 test different scenarios. The interest in tracking aquaculture wastes with mathe-
74 matical models has been rapidly increasing in time as a consequence (Henderson
75 et al., 2001). In the past we have moved from using analytical models describing
76 oversimplified dispersion patterns in a constant flow in time and space (Gowen et al.,
77 1989), to implementing equations with too many simplifying assumptions about hy-
78 drodynamics (Gillibrand & Turrell, 1997). Others have developed particle tracking
79 models using hydrographic data and were therefore limited in their simulations by
80 the sparse data in time and in space (Cromey et al., 2002). Ocean dynamics, instead,
81 are usually very complex and ocean ecosystems are likely to experience current re-
82 versals and flow variability. Pioneering numerical studies used circulation models
83 focusing on strongly tidally driven systems. In this case, the flow could have been
84 considered obeying two-dimensional (2D) vertically averaged dynamics (Panchang
85 et al., 1997; Dudley et al., 2000). Unfortunately, the 2D approximation can be
86 inappropriate in more complex and dynamical systems where vertical phenomena
87 affect the dispersion of different particles. Having this in mind, some of us were the
88 first ones to directly take into account the three-dimensional (3D) ocean circulation
89 and its variability in tracking different aquaculture wastes (Doglioli et al., 2004a).
90 Nevertheless, to our knowledge, Doglioli et al. (2004a) (hereinafter referred to as
91 DMVT04) still represents the only application of a 3D hydrodynamical model for
92 aquaculture purposes.

93 The present study takes place following the continuous effort in improving the
94 framework initially set up by DMVT04. The improvements and the assessment of
95 their relative importance have been done mainly in three areas and represent the
96 core and the original intent of this work. Namely, in this study we (a) improved our

97 hydrodynamics using real historic current-meter data to force the simulations; (b)
98 improved our dispersion using a larger number of particles and updating the settling
99 velocity values specifically for Mediterranean fish species and for their feed; and (c)
100 added a new coupled benthic module to consider the environmental response to the
101 organic load from the cages.

102 In DMVT04 some of us used idealized winds to force simulations. The choice
103 of the winds was based on a statistical treatment of 34 years of wind data and it
104 allowed us to carry out a complete 12-day hydrodynamic simulation during which
105 wind direction and speed were changing according to a typical local meteorological
106 sequence. In a later paper, however, some of us successfully used historical current-
107 meter data to study the hydrodynamic characteristics of the area under examination
108 (Doglioli et al., 2004b). Since the focus of this study is to move toward a more
109 realistic scenario, we decided to implement the already validated forcing setup used
110 in Doglioli et al. (2004b). This mainly implies that the open boundary conditions
111 and the forcing evaluation are improved by applying realistic current measurements.

112 On the other hand, settling velocity values for uneaten feed and faeces represent
113 key parameters for aquaculture waste dispersion models. The lack of values specifi-
114 cally targeting Mediterranean fish and their feeds obliged DMVT04 to use the only
115 values available in the literature, i.e. the ones measured for salmonids (Chen et al.,
116 1999a,b). However, two recent works filled this important gap. On one side, some of
117 us, in Vassallo et al. (2006) presented the settling velocities of a feed usually utilized
118 in Mediterranean farms (the ‘Marico Seabass and Seabream’ pellets produced by
119 Coppens International), while on the other side, Magill et al. (2006) measured the
120 settling velocities of Gilthead Sea Bream and Sea Bass faecal particles collected in
121 sediment cores in a Greek fish farm. A second original aspect of this study is that
122 it uses these new values, paying particular attention to the role they play in the
123 overall results.

124 Finally, we recognize that following only the fate of the particles as we did in

125 DMVT04 is not sufficient to correctly assess the organic load on the sea bottom. The
126 modeling effort should consider the natural capability of the benthic environment
127 in reacting and absorbing fluctuations in the organic load. Our model framework
128 is integrated with an additional new numerical benthic degradative module, the
129 Finite Organic Accumulation Module (FOAM). FOAM is mainly based on the ideas
130 expressed in the work of Findlay & Watling (1997) (hereinafter referred to as FW97).
131 They proposed an index of impact based on the ratio between the quantity of oxygen
132 supplied to the sediment and the quantity of oxygen demanded by the sediment.
133 **The oxygen supply is a function of the near bottom flow velocities and**
134 **is calculated by the empirical relation put forth by FW97.** The oxygen
135 demand is based on the organic load from the cages and it is strongly related to
136 the microbial benthic metabolism rate. As pointed out by the same authors, the
137 equations proposed by FW97 can be easily exploited by numerical modelers since
138 the only needed input variables are the bottom flow velocities and the organic flux
139 toward the seabed. Since our model does consider the vertical dimension, it is also
140 able to provide these important required data. Furthermore, its intrinsic Lagrangian
141 nature allows a simple numerical implementation of the ideas proposed in FW97.

142 The rest of this paper is organized as follows. In Section 2 a description of the
143 study area and the details of the modeling effort are provided. The results of the
144 numerical experiments are presented in Section 3 and discussed in Section 4. Finally
145 the conclusions are given in Section 5.

146 **2 Methods**

147 The simulations are carried out for the offshore fish farm located in the Ligurian Sea
148 already described in DMVT04 (Fig. 1). The sea cages are located at about 1.5 km
149 from the coast and they cover an area of 0.2 km². The bottom depth ranges between
150 38 m and 41 m. The farm is composed of 8 fish cages with a capacity of 2000 m³

151 each. The reared biomass is 20 kg m^{-3} for an annual mean production of about
152 200 ton year⁻¹. The fish in the cages are Gilthead Sea Bream (*Sparus aurata*) and
153 Sea Bass (*Dicentrarchus labrax*).

154 The modeling framework consists of different models which are coupled together
155 into a single functional unit (Fig. 2). The hydrodynamic model is the Princeton
156 Ocean Model (POM) and it is used to derive space and time information of the
157 circulation of the coastal area. POM is coupled online with the three-dimensional
158 Lagrangian Assessment for Marine Pollution Model (LAMP3D). LAMP3D is used
159 to track the particle positions in time and space. The Finite Organic Accumulation
160 Model (FOAM) represents the biochemical component of the modeling system and
161 it uses POM and LAMP3D outputs to estimate the potential environmental impact
162 due to the organic load from the cages. POM and LAMP3D calculate the bottom
163 velocities and the particle fluxes to the bottom and these values are then used by
164 FOAM to calculate the final organic load in each mesh of its numerical domain.

165 The following part of this section gives a more detailed description of the entire
166 modeling framework.

167 **2.1 The advective and dispersive models: POM and LAMP3D**

168 Some historical measurements of the coastal current in the area are available in
169 terms of current-meter time series and hydrographic surveys, covering a total of
170 10 months during 1978 - 1979 (Astraldi & Manzella, 1983). Data are archived in
171 the SIAM database (<http://estexp.santateresa.enea.it/www/siams/prov102.html>), and they have been kindly provided to us by the Italian National Agency
172 for New Technologies, Energy and Environment (ENEA) and the National Research
173 Council (CNR). In this study, we concentrate on the winter-spring period, when
174 the currents are stronger and better defined and the stratification is being formed.
175 We select the period from February 8th 1979 to June 30th 1979 and we force the
176 model on the eastern boundary. At the western boundary a radiation condition
177

178 is imposed. The described setup is the same used and validated in Doglioli et al.
179 (2004b). The reader is referred to this paper for a more detailed description of the
180 boundary conditions and for their validation. Here, complete four-month simulations
181 are carried out, obtaining current data necessary for the dispersion-degradation runs.
182 The first velocity value ($U = -0.19 \text{ m s}^{-1}$), measured on February 8th 1979, is
183 provided on the whole domain as an initial condition for all the simulations. Since
184 the objective of this work is simulating longer time periods, we cyclically repeat the
185 real current-meter data as boundary conditions to force the runs. Consequently, the
186 organic matter accumulation on the seabed can be estimated for longer time periods
187 and the dependence of the model results on the initial condition can be reduced.

188 Moreover, since the primary focus of this study is the organic load on the seafloor
189 and not the fate of the dissolved nutrients, we adopt a new setup with respect to
190 that used in DMVT04 for the hydrodynamical model POM and the dispersive model
191 LAMP3D (see Fig. 1). The POM grid has 115×80 meshes with a spatial resolution
192 of 400 m along the x -direction and 200 m along the y -direction. **This resolution**
193 **reflects the best available bathymetric data in the area.** The LAMP3D
194 numerical domain, instead, is smaller ($8 \text{ km} \times 4 \text{ km}$), and it is nested in the POM
195 grid with the same spatial resolution ($400 \text{ m} \times 200 \text{ m}$).

196 The other dispersive parameters are unchanged with respect to DMVT04, with
197 the exception of the Lagrangian particle number that was increased to 620000 for
198 greater precision and better rendering. The DMVT04's assumptions on the organic
199 carbon concentration in feed and faecal waste are adopted. In particular, the value
200 of 5% for the feed loss was recently confirmed by results of MERAMED project
201 (<http://www.meramed.com>). Nevertheless, since the number of particles is increased
202 with respect to DMVT04, we calculate new conversion factors for uneaten feed and
203 faecal waste (Table 1). We also keep calculating nitrogen loading rates for validation
204 purposes (see Section 3) using the same conversion factors used in DMVT04 for
205 nitrogen.

206 The lack of data for Mediterranean species obliged us in DMVT04 to use the
207 values proposed by Chen et al. (1999a) and Chen et al. (1999b) for salmonids. Re-
208 cently Magill et al. (2006) have measured the settling rates of faecal material of
209 Gilthead Sea Bream and Sea Bass, while, under laboratory conditions reproducing
210 the Mediterranean sea water, Vassallo et al. (2006) have provided the settling ve-
211 locity values of a typical growing sequence of feed pellets for the same species. We
212 therefore used the values of these recent works in our simulations.

213 All the parameters used in the hydrodynamic and dispersive models are sum-
214 marized in the upper part of Table 1, while the different settling velocity values are
215 reported in Table 2.

216 **2.2 The benthic module: FOAM**

217 A new bottom boundary condition is implemented in our model. When a numerical
218 particle touches the seabed, it is considered as biodegradable settled matter and
219 it is treated by the benthic module FOAM. FOAM covers the same area of the
220 dispersive model but its resolution is 10 times higher, namely $40\text{ m} \times 20\text{ m}$ (Fig. 1).
221 **This resolution adequately represents the known processes of degradation**
222 **and is acceptable in terms of computational time. In the case of FOAM,**
223 **a higher resolution is feasible because its calculations are performed off-**
224 **line.**

225 According to FW97, the organic accumulation on the bottom leads to different
226 rates of mineralization in relation to the level of stress the seabed is exposed to.
227 In order to simulate the biological reaction of the microbial benthic community to
228 the variations in the organic enrichment, we assign the status of the sediment in
229 each grid mesh according to the ratio between the benthic oxygen supply and the
230 demand.

231 **In FOAM the same equations and constants proposed by FW97 are**
232 **used.** The oxygen supply is a function of the near bottom velocities and can be

233 calculated by simple Fickian diffusion arguments and expressed by the empirical
 234 relation

$$235 \quad \text{O}_2^{sup} = A + B \cdot \log(\bar{v}) \quad (1)$$

236 where A and B are constants (see Table 1) and \bar{v} is a time averaged current velocity
 237 taken at 1 m from the bottom. It is important to note that \bar{v} is just the numerical
 238 value of the bottom flow velocity when it is expressed in cm s^{-1} . In our model
 239 this value is obtained by linear interpolation of the velocity in the deepest vertical
 240 grid cell and by using an average time interval of $\Delta t = 2$ hours. This choice was
 241 already made by FW97 to describe oxygen supply to the benthos. Moreover, this
 242 time interval seems to be critical, since a 2 hour exposure to reduced oxygen and
 243 elevated hydrogen sulfide concentrations causes permanent damage to the gill tissues
 244 of sensitive infauna (Theede et al., 1969). The same choice of $\Delta t = 2$ hours is also
 245 supported by the more recent work by Morrissey et al. (2000).

246 The oxygen demand, instead, is a function of the organic carbon flux toward the
 247 sea bottom Flx^{Bot} according to the relation

$$248 \quad \text{O}_2^{dem} = C \cdot Flx^{Bot} + D \quad (2)$$

249 where, again, C and D are just constants (Table 1; **for more details refer to Fig.**
 250 **2 and Fig. 3 in FW97**). If i and j are the grid mesh indexes in the x and y
 251 directions respectively, the carbon flux Flx^{Bot} in each grid mesh (i, j) at the instant
 252 k is calculated on the basis of the number of particles reaching the bottom, $n_{i,j}^{Bot}$,
 253 during an integration time interval dt , i.e.

$$254 \quad Flx_k^{Bot} = \frac{n_{i,j}^{Bot} \cdot w^C}{dt \cdot \Delta x \cdot \Delta y} \quad (3)$$

255 In the equation (3), Δx and Δy are the horizontal grid sizes while w^C stands
 256 for the adopted organic carbon conversion factor. w^C varies if we consider feed or
 257 faeces and the different values are listed in Table 1.

258 Once the model provides O_2^{sup} and O_2^{dem} for each grid mesh, we can calculate the

259 index of impact I as suggested by FW97 as

$$260 \quad I_{i,j} = \frac{O_2^{sup}}{O_2^{dem}} \quad (4)$$

261 Based on I we can identify three different levels of stress: non-stressed sediments,
 262 intermediately-stressed sediments and highly-stressed sediments. FW97 suggested
 263 that when $I > 1$, the supply of oxygen is in excess of the demand and therefore the
 264 impact is minimal. When $I \approx 1$ the impact can be moderate while when $I < 1$, the
 265 sediment exhibits the azoic sediment endpoint and the resulting impact is high. In
 266 our model the discrete FW97 criterion for the different levels becomes

- 267 · no stress, if $I_{i,j} > 1 + \Delta_{fw}$;
- 268 · medium stress, if $(1 - \Delta_{fw}) \leq I_{i,j} \leq (1 + \Delta_{fw})$;
- 269 · high stress, if $I_{i,j} < 1 - \Delta_{fw}$.

270 Sensitivity tests on the Δ_{fw} parameter are performed in a range varying from $\Delta_{fw} =$
 271 0.05 to $\Delta_{fw} = 0.5$. We observe no meaningful differences, so, for precautionary
 272 reasons, the value of $\Delta_{fw} = 0.5$ is adopted.

273 When the level of stress is decided according to the value $I_{i,j}$, different rates of
 274 mineralization are used in each grid mesh. In our code, this is obtained by sub-
 275 tracting different quantities to the already calculated organic carbon concentration
 276 fluxes. The subtracted amounts are the same as FW97 and are shown in the lower
 277 part of Table 1. On the basis of the obtained fluxes, the organic carbon concentra-
 278 tion $Conc^{Bot}$ in each grid mesh (i, j) is calculated as

$$279 \quad Conc^{Bot} = \sum_{k=1}^{NT} Flux_k^{Bot} \cdot dt \quad (5)$$

280 where NT is the number of the time intervals of the simulation.

281 All the parameters used in the benthic module are summarized in the lower part
 282 of Table 1.

3 Results

The modeled water circulation is in agreement with the past literature in the area: the simulations show the presence of the observed westward transport (Astraldi & Manzella, 1983; Astraldi et al., 1990), persisting for almost the entire simulated period (winter-spring). The obtained general circulation also agrees with other numerical experiments such as Baldi et al. (1997) and DMVT04. It is also possible to observe current separation and eddy formation behind the Portofino Promontory as in Doglioli et al. (2004b). For a more quantitative hydrodynamic validation, we use the same approach as in DMVT04. Current data simulated by the model are compared with data collected by one current meter, C1, located at 2 km to the west of the farm. Current speed and direction were sampled every hour at 20-m depth from February 1993 to March 1994. Table 3 shows current data from C1 and the model outputs. When we use only one cycle at the eastern boundary and we prescribe the first velocity value on the whole domain as an initial condition, the seasonal averages from the observations are systematically lower than the model ones (see values for the first cycle). When we cyclically repeat the boundary conditions to force the runs and we use as the initial condition the last velocity field of the previous cycle, the comparison with the C1 data improves (see values for the fifth cycle). We speculate that the larger discrepancy observed in the first cycle is due to the artificial highly energetic initial condition. Therefore, we decide to run five cycles of linked simulations and we subsequently neglect the first two in order to reduce the sensitivity to the initial conditions. The three linked cycles account for a total of 430 simulated days and their averages are also reported in Tab. 3. In this case, the data are very close to the values calculated by the model. Current direction agrees with the observed along-shore water movement. Sporadic current reversals are also simulated thanks to the inversions of the direction of the velocity at the inflow boundary condition.

At the same time, we can use sediment observations around the cages to validate

311 our dispersive runs. A Van Veen grab was used to collect sediment samples in three
312 repetitions in each of the four stations surrounding the fish farm (see **Fig.7 of**
313 **DMVT04 for the exact location of the sampling stations**). With respect
314 to DMVT04, additional recent data were collected in the same stations. All the
315 samples were analyzed for total nitrogen and total phosphorus. The comparison
316 between absolute values of these data and the model outputs is not possible since,
317 in order to express both of them in the same units, we would need to make strong
318 assumptions on the sediment density as well as on the sampling methodology. We
319 therefore use the same approach used in DMVT04. Fig. 3 shows the agreement
320 between the field and modeled data. In particular, field sediment nutrients are
321 highest in station S2 and lowest in station S4, which agrees with model output for
322 total nitrogen under westward transport. To facilitate the comparison of results
323 for the reader, in the same Fig. 3, we also show the performance of the old setup
324 adopted in DMVT04 and the field data as they were at that time.

325 The above comparison with the only data available in the area, allows us to
326 focus on the dispersion model and on the benthic modeled impact. The time series
327 of the dispersion model output are also referred to the three last cycles of linked
328 simulations. In order to explore the differences in the runs by varying waste typology,
329 release condition and settling velocity, we set up the following experiments:

- 330 A1) slowly sinking feed in continuous release;
- 331 A2) quickly sinking feed in continuous release;
- 332 B1) slowly sinking feed in periodical release;
- 333 B2) quickly sinking feed in periodical release;
- 334 C1) slowly sinking faeces (continuous release);
- 335 C2) quickly sinking faeces (continuous release).

336 Note that for periodical release we mean that the feed is supplied twice a day, and
 337 slowly and quickly sinking are referred to the minimum and maximum values listed
 338 in Table 2 for the two different waste typologies. In Table 2 the slowly sinking values
 339 are indicated with a single arrow pointing toward the bottom (\downarrow), while the quickly
 340 sinking values with a double one (\Downarrow).

341 Results from the benthic module are presented in relation to (i) the extension
 342 of the impacted area, (ii) the position of this area in terms of its barycenter, (iii)
 343 the benthic trophic conditions and (iv) the predicted organic concentration at the
 344 barycenter. The choice of these parameters allows the simple and objective estima-
 345 tion of the degree and the location of the potential impact.

346 The impacted surface S is the sum of the areas of the grid meshes where particles
 347 are still present even after the benthic degradation activity. The position of the
 348 barycenter (x_b, y_b) of this area is basically a position weighted by the number of
 349 particles left in each cell after the degradation. It is simply expressed as

$$350 \quad x_b = \frac{\sum_{j=1}^N \sum_{i=1}^M i \cdot n_{i,j}^{left}}{n_{Tot}^{left}} \quad (6)$$

$$351 \quad y_b = \frac{\sum_{j=1}^N \sum_{i=1}^M j \cdot n_{i,j}^{left}}{n_{Tot}^{left}} \quad (7)$$

352 where M and N are the numbers of meshes in the x and y directions, $n_{i,j}^{left}$ is the
 353 number of particles left on the bottom in the mesh (i, j) and $n_{Tot}^{left} = \sum_{j=1}^N \sum_{i=1}^M n_{i,j}^{left}$
 354 is the total number of particles left on the bottom after the degradation. The
 355 benthic trophic condition and the predicted organic concentration at the barycenter
 356 are simply given by the parameter I and $Conc^{Bot}$ in the grid mesh corresponding
 357 to the barycenter position.

358 We initially describe the effects on the extension of the impacted area. Fig. 4
 359 shows the time series of the calculated extensions in the different experiments and
 360 the temporal variations of the modeled current velocity near the cages (Fig. 4D).
 361 The slowly sinking feed particles continuously released (Fig. 4A, solid black line) are

362 dispersed by the current a little bit more than the quickly sinking ones (dashed gray
363 line). This is also confirmed by the time averages and the standard deviations for
364 the experiments A1 and A2 (see Table 4). The situation changes when we consider
365 periodical release (Fig. 4B). In this case both slowly and quickly sinking particles
366 are dispersed on a larger area than in the continuous case. However, while for
367 slowly sinking particles this area is much larger and less variable in time than in the
368 continuous release, for quickly sinking ones, the area is just a little bit bigger and
369 more variable (see Table 4). The variability of the dispersion is therefore associated
370 with the current velocity and it increases both with periodical release and with
371 decreasing settling velocity values. For faecal pellets (Fig. 4C), the impacted area
372 is smaller than in the previous cases. Moreover, faecal wastes show greater time
373 variability than the uneaten feed, no matter what the feed release is. The slowly
374 sinking faecal particles impact smaller areas with respect to the quickly sinking ones,
375 and also the variability is smaller than the quickly sinking ones (Table 4).

376 Fig. 5 gives a better visualization of what has been stated so far and, at the
377 same time, it shows the position of the barycenter of the impacted area. In this
378 figure, we schematize the extension of the impacted area with a circle centered in
379 the barycenter and having an area equivalent to the one already calculated. The gray
380 scale represents the time evolution of the results every sixty days, while a circle is
381 drawn every ten days. In the case of feed, for both continuous and periodical releases,
382 the barycenter of the impacted area is found at approximately 25 m southwestward
383 from cages. For the same simulations, a less significant time variability is observed
384 (Fig. 5A1, A2, B1 and B2) and this means that the impacted area is always larger
385 and that higher stress levels are expected. In the case of faecal wastes, instead, the
386 barycenter shows greater time variability, according to changes in current direction
387 and intensity (Fig. 5C1 and C2). This variability results in a dispersion of the faecal
388 particles in different areas and therefore lower stress levels are expected.

389 To better emphasize these results, we can look at the scatter diagram of the

390 parameter I at the barycenter position in time (Fig. 6). For clarity, all values greater
391 than 2 are artificially assigned to 2 in this figure. For feed particles continuously
392 released (Fig. 6A), I mainly stays in the non-stressed range (i.e. $I > 1.5$), sometimes
393 goes up to the intermediately-stressed range, but the highly-stressed level is rarely
394 reached. There is a slight tendency for quickly sinking particles to stay more in the
395 intermediate regime than the slow ones (Table 4). For periodical release (Fig. 6B),
396 I is often in the non-stressed range, very rarely in the intermediately-stressed range
397 but it reaches the highly-stressed level more frequently than before. An easy and
398 quick check shows that the highly-stressed values are registered, in this case, in the
399 period going from 2 to 4 hours after the release. No significant difference can be
400 observed between slowly and quickly sinking particles. For faecal wastes (Fig. 6C),
401 the parameter I is practically always greater than 2 (for this reason in the plot all
402 dots are squeezed in the top) for both slowly and quickly sinking particles.

403 Finally, the mean values of the computed organic matter concentration $Conc^{Bot}$
404 remaining on the seabed at the barycenter position after the degradation are re-
405 ported in the last column of Table 4. The organic carbon amount due to feed waste
406 almost linearly increases with time and the maximum values are reached in the case
407 of the most quickly sinking feed particles in periodical release. The faecal waste in-
408 stead seems to be completely degraded and it does not contribute to organic carbon
409 concentration at the bottom.

410 All the results are summarized in Table 4.

411 **4 Discussion**

412 The new model setup is shown to better reproduce both the hydrodynamics and the
413 dispersion in the investigated area. This is mainly due to the new forcing which is
414 based on current meter data and leads to more realistic results. As already remarked
415 in previous works, current direction and intensity strongly influence the position of

416 the impacted area and the degradation of the settled matter (FW97, Morrisey et al.,
417 2000). Nevertheless, the processes involved are strongly non-linear and it is difficult
418 to assess the role played by each parameter in the model.

419 When particles sink relatively quickly (settling velocities are one order of magni-
420 tude less than the current velocity, as a lower limit) the impacted area does not vary
421 and the barycenter position depends on the main direction of the current. Instead,
422 for relatively slowly sinking particles, the variability of the current starts to play a
423 major role. This different behavior explains why the barycenter of the uneaten feed
424 remains practically motionless, while the one for the faeces is very mobile.

425 At the same time, current intensity reduces bottom degradation thanks to two
426 different processes. On one hand, a stronger current brings more oxygen to the sed-
427 iment and makes degradation more efficient. On the other hand, the same stronger
428 current increases waste dispersion resulting in a wider impacted area and in lower
429 waste concentrations on the bottom. Faeces do not contain much organic carbon
430 and the strong degradation is able to remove almost all the settled matter. Uneaten
431 feed contains more organic carbon and sinks more rapidly than faeces. As a result,
432 much more carbon accumulates on the sea floor and it is only partially degraded
433 even in presence of strong currents. This also explains the observed small variability
434 of the size and position of the impacted area.

435 Since we use the settling velocity values for faeces measured by Magill et al.
436 (2006), it is particularly interesting to compare our results with theirs. In order to
437 do this, we calculated the accumulation rates in the barycenter for different sinking
438 faeces. We obtained values of $11 \text{ g faeces m}^{-2} \text{ year}^{-1}$ and $19 \text{ g faeces m}^{-2} \text{ year}^{-1}$ for
439 slowly and quickly sinking particles, respectively. These values are about two orders
440 of magnitude smaller than the ones reported in Magill et al. (2006). Two arguments
441 can be provided to explain this discrepancy. Firstly, the total fish biomass in the
442 cages is not reported in Magill et al. (2006) and this does not allow for a correct
443 quantitative comparison. The policy of the fish farm studied in this work is to

444 keep low biomass per cage (Roberto Co', AQUA s.r.l., personal communication).
445 It is likely that the Greek fish farm studied by Magill et al. (2006) has a high
446 biomass value per cage. Secondly, with the new module FOAM, we introduced the
447 degradation of the settled organic carbon which is not considered instead by Magill
448 et al. (2006). However, since we adopted the degradation rates proposed by FW97
449 for Atlantic fish farm, it is also possible that these values are too high with respect
450 to the Mediterranean ones. Unfortunately, to the best of our knowledge no value
451 is available in literature to check if this is really the case. On the other hand, our
452 results agree with the work of Magill et al. (2006) in predicting a greater impact for
453 the faeces of *D. Labrax* respect to *S. Aurata*'s ones. The same results also agree with
454 previous studies and confirm the uneaten feed to be the primary cause of ecological
455 impact on the benthos community (Beveridge et al., 1991; Vezzulli et al., 2003).
456 For this reason, we studied in more detail the feed release conditions. We found
457 that a release occurring twice a day results in i) more frequent conditions of highly-
458 stressed sediments and ii) larger impacted areas than a continuous release. These
459 results support the idea already proposed in previous studies of using self-feeders
460 to reduce the uneaten feed loss without affecting fish growth rates (Azzaydi et al.,
461 1998, and references therein).

462 5 Conclusions

463 Aquaculture is the food-related activity with the most rapid growth in the world.
464 Since this growth produces an immediate concern, it is necessary to develop tools
465 to predict the environmental impacts coming from intensive marine fish farms.

466 In this study we improved the capability of the POM-LAMP3D model already
467 proposed in a previous work (Doglioli et al., 2004a). We developed both a more
468 realistic advection-dispersion setup and a new benthic model, the Finite Organic
469 Accumulation Module (FOAM). Using the empirical relations put forth by Findlay &

470 Watling (1997), FOAM calculates the organic carbon degradation for three different
471 levels of sediment stress. We performed several runs to simulate different scenarios
472 by varying waste typology (faecal or feed), settling velocity of particles (on the
473 basis of feed dimensions, fish size and reared species) and release conditions of feed
474 (periodical or continuous). **At the same time, the same runs allowed us to**
475 **test the stability of the model which appears very satisfactory.**

476 We obtained more satisfactory results for the hydrodynamics and dispersion than
477 in Doglioli et al. (2004a). Moreover, FOAM revealed its ability to simulate different
478 scenarios by switching suitable parameters.

479 The results presented in relation to the extension of the impacted area and the
480 position of its barycenter show that the continuously released feed settles within
481 a narrow area near the cages (impact area maximum 6500 m²; barycenter shifting
482 amplitude 10 m; cages maximum distance 25 m); while the feed released twice a day
483 spreads on a larger area centered near the cages (maximum area 8500 m²; barycenter
484 shifting amplitude 15 m; cages maximum distance 25 m). Faecal pellets accumulate
485 on a smaller area within a greater and more variable range from the cages (maximum
486 area 4000 m²; barycenter shifting amplitude 100 m; cages maximum distance more
487 than 50 m) with respect to uneaten feed. Maximum impacts, in terms of both stress
488 parameter I and organic carbon concentration are due to the quickly settling feed,
489 released in periodical mode and during slow current periods. Some mitigation of
490 the impact is observed if feed is continuously released. The use of self-feeders has
491 therefore been suggested to the farmers.

492 Further investigations may be necessary to verify the impact of combined feed
493 and faeces settling, while mineralization rates for Mediterranean conditions and
494 validation with specific in-situ measurements are required.

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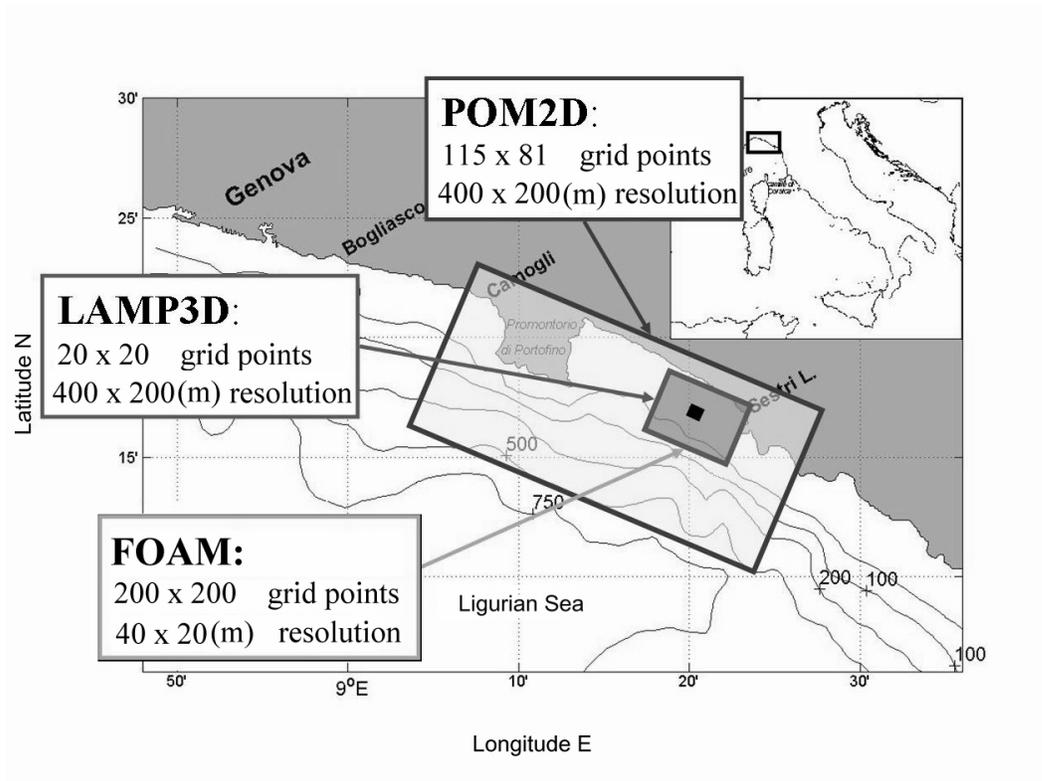


Figure 1:

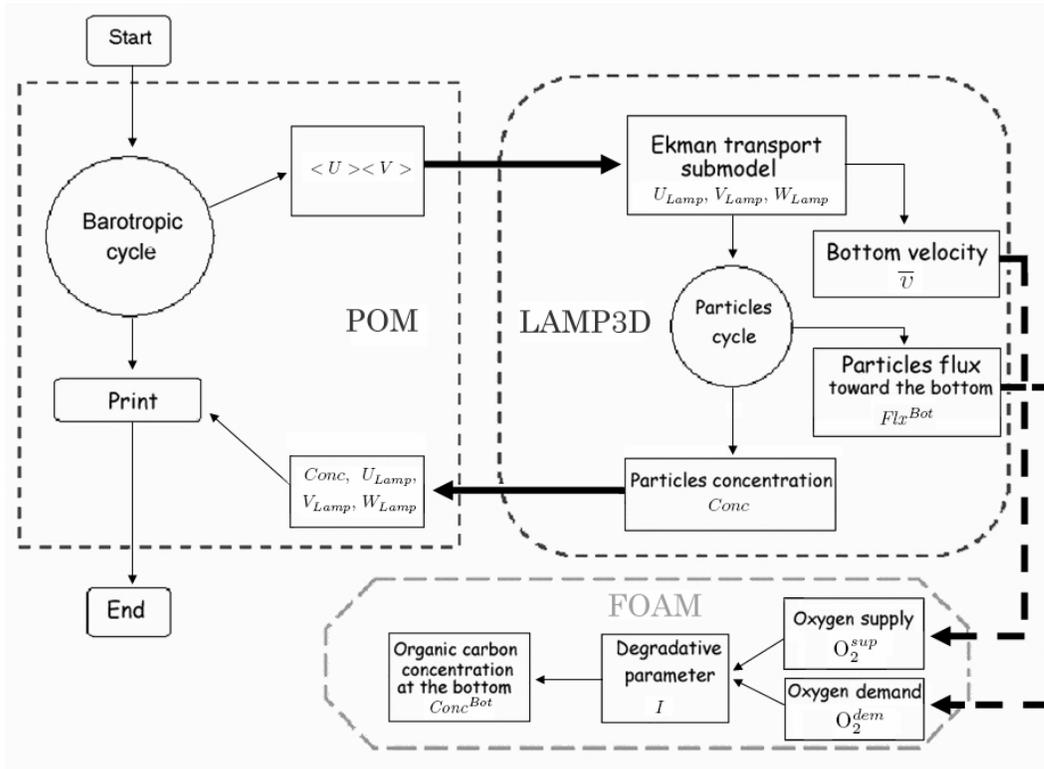


Figure 2:

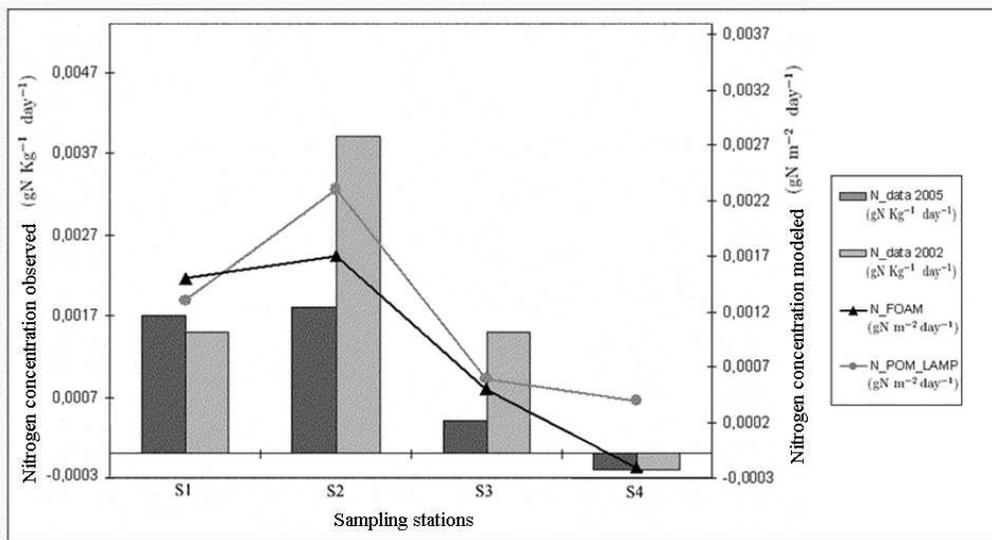


Figure 3:

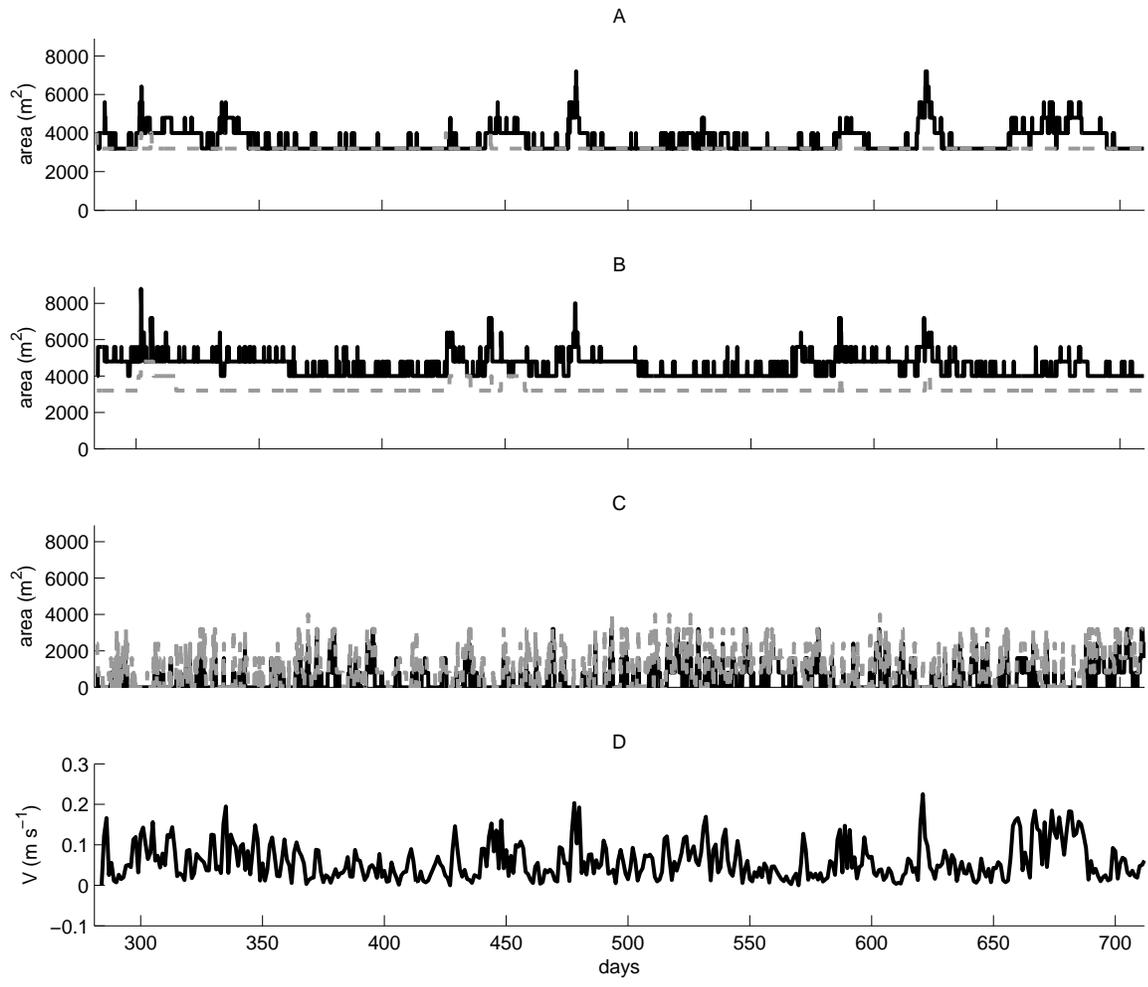


Figure 4:

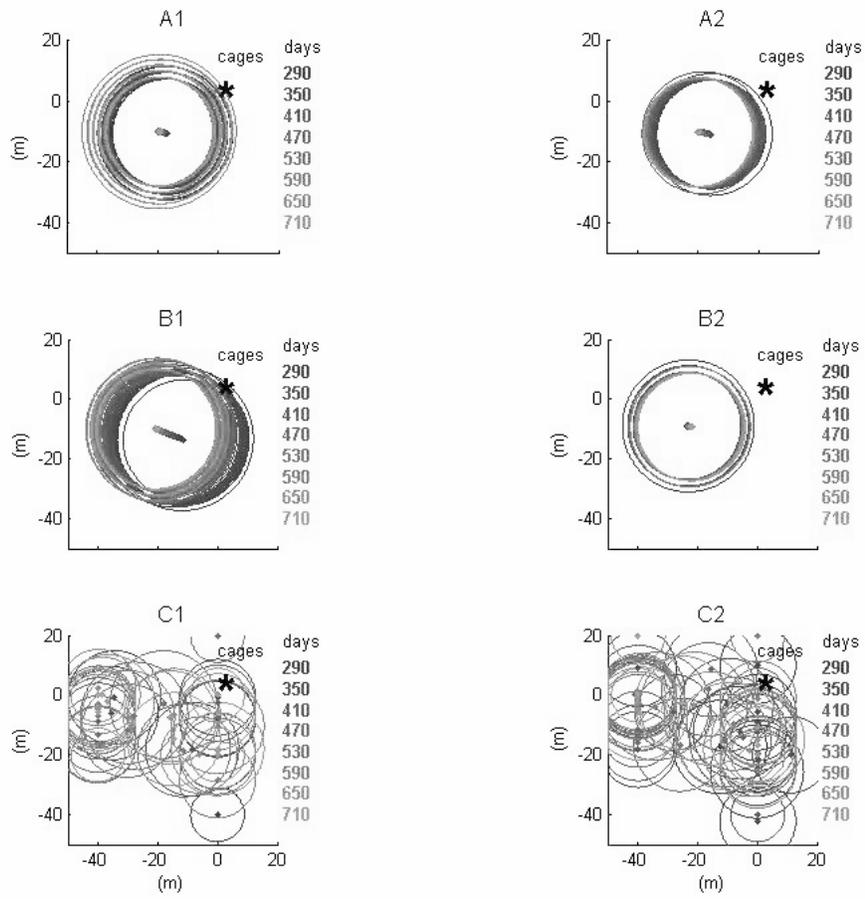


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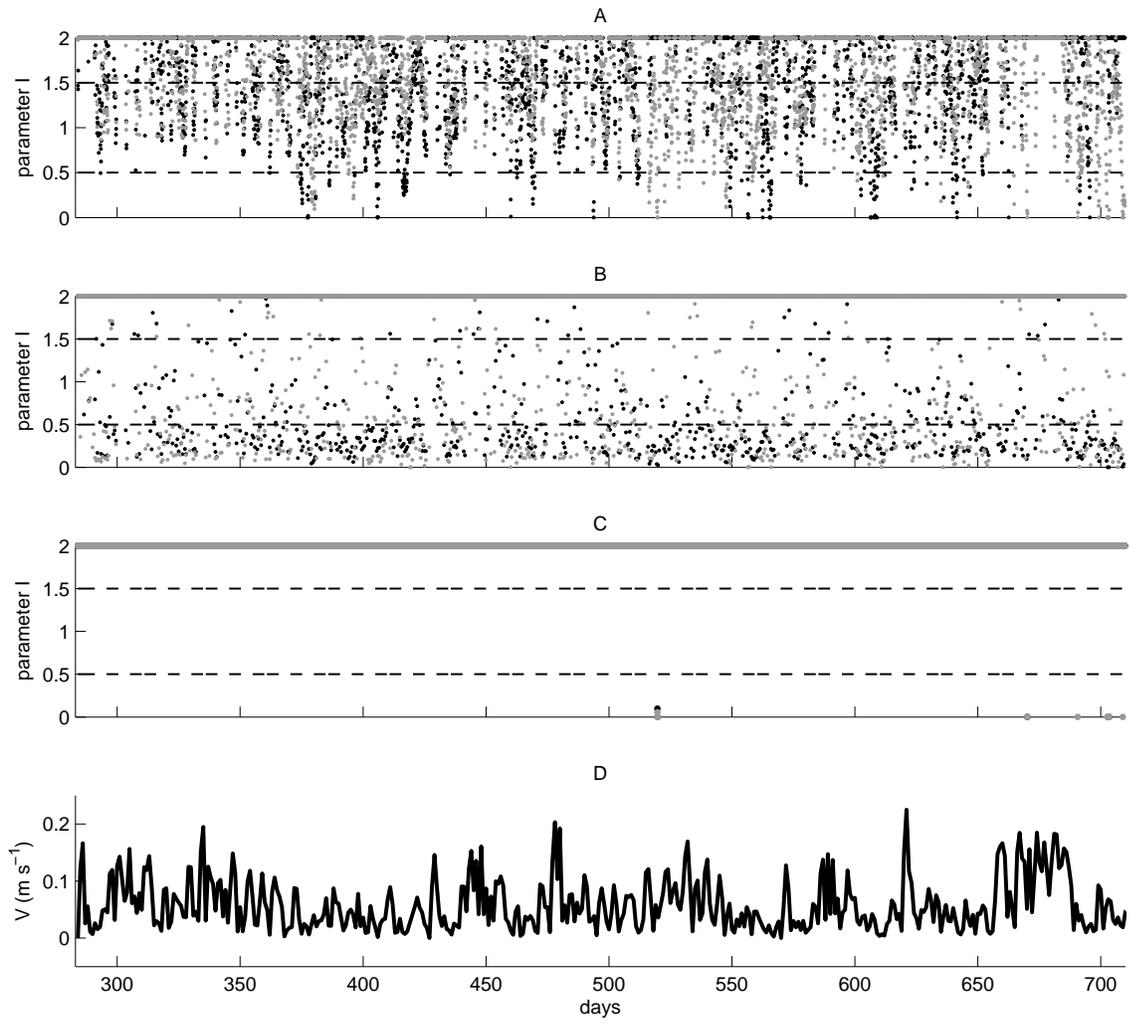


Figure 6:

POM-LAMP3D parameters	value
POM physical domain (km)	46x16
LAMP3D physical domain (km)	8x4
Horizontal resolution (m)	400x200
Vertical resolution (m)	10
Barotropic cycle time step (s)	1
Smagorinsky diffusivity coefficient	0.1
Asselin filter coefficient	0.05
Ekman depth δ_E (m)	50
Wind drag coefficient C_d	0.001
Horizontal standard deviation σ (m)	3.46
Particle cycle time step (s)	60
Number of particles	620000
Feed conversion factor for organic carbon w_{feed}^C (mmolC particle ⁻¹)	308.6
Faeces conversion factor for organic carbon w_{faeces}^C (mmolC particle ⁻¹)	5.8
Feed conversion factor for nitrogen w_{feed}^N (mmolN particle ⁻¹)	167.8
Faeces conversion factor for nitrogen w_{faeces}^N (mmolN particle ⁻¹)	66.4
FOAM parameters	value
Physical domain (km)	8x4
Horizontal resolution (m)	40x20
O_2 supply parameter A (mmolO ₂ m ⁻² d ⁻¹)	736.3
O_2 supply parameter B (mmolO ₂ s m ⁻³ d ⁻¹)	672.5
O_2 demand parameter C (mmolO ₂ mmolC ⁻¹)	1.07
O_2 demand parameter D (mmolO ₂ m ⁻² d ⁻¹)	-32.6
Settled matter non-stress N_s (mmolC m ⁻² d ⁻¹)	27.53
Settled matter intermediate-stress I_s (mmolC m ⁻² d ⁻¹)	57.50
Settled matter hyper-stress H_s (mmolC m ⁻² d ⁻¹)	30.59
I range amplitude parameter Δ_{fw}	0.5

Table 1:

Feed pellets		Faecal pellets	
Diameter (mm)	V_{sed} (m s ⁻¹)	Fish species [size (g)]	V_{sed} (m s ⁻¹)
3	0.087 ↓	<i>S. Aurata</i> [380]	0.004 ↓
3.5	0.118	<i>S. Aurata</i> [60]	0.005
4.5	0.103	<i>D. Labrax</i> [280]	0.006
5	0.144 ↓	<i>D. Labrax</i> [80]	0.007 ↓
6	0.088		

Table 2:

Observations (m s^{-1})					
	Winter average (std)	Spring average (std)	Summer average (std)	Autumn average (std)	Annual average (std)
C1	0.066 (0.057)	0.075 (0.065)	0.063 (0.052)	0.070 (0.052)	0.069 (0.057)
Model Output (m s^{-1})					
	Winter average (std)	Spring average (std)	Summer average (std)	Autumn average (std)	Overall average (std)
1st cycle	0.076 (0.051)	0.103 (0.084)	- -	- -	0.088 (0.047)
5th cycle	0.059 (0.034)	0.082 (0.066)	- -	- -	0.057 (0.034)
3th \rightarrow 5th cycles	0.064 (0.042)	0.078 (0.050)	- -	- -	0.061 (0.034)

Table 3:

Exp.	Simulation typology (release)	<i>S</i> Impacted area mean \pm std (m ²)	Parameter <i>I</i>			Organic concentration mean \pm std (gC m ⁻²)
			no stress (% days)	medium stress (% days)	high stress (% days)	
A1	Slow feed (continuous)	3576 \pm 582	74	22	4	1450 \pm 404
A2	Quick feed (continuous)	3202 \pm 41	71	27	2	1490 \pm 453
B1	Slow feed (periodical)	4513 \pm 563	87	4	9	895 \pm 380
B2	Quick feed (periodical)	3277 \pm 266	88	4	8	1590 \pm 387
C1	Slow faeces	377 \pm 656	99	0	1	< 1
C2	Quick faeces	941 \pm 962	99	0	1	< 1

Table 4: