

# 1 FOAM, a new simple benthic degradative 2 module for the LAMP3D model: an 3 application to a Mediterranean fish farm

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## Abstract

The modeling framework already introduced by (Doglioli et al., 2004a) to predict the potential impact of a marine fish farm is improved following different directions. Namely: (i) real historic current-meter data are used to force the simulations; (ii) settling velocity values specifically targeting Mediterranean fish species are used; and (iii) a new benthic degradative module, FOAM, is added to the modeling framework. FOAM uses the output of the other functional units of the modeling framework to calculate the organic load on the seabed at the net of the natural remineralization. Different remineralization rates reflect the sediment stress level according to the work of Findlay & Watling (1997).

Organic degradation for both uneaten feed and faeces is evaluated changing release modality (continuous and periodical) and varying the settling velocities. It is found that the maximum impact on the benthic community is observed either for quickly-sinking uneaten feed released twice a day or for less intense near bottom current conditions. If both the above mentioned scenarios coexist, a high stress level is established in the sediment. The model also suggests that a demand-feeding of the fish in the cage can significantly reduce the farm impact. These results show how the new and more complete modeling framework here presented is able to improve the objectivity in decision making processes and it may be successfully used for planning and monitoring purposes.

# 1 Introduction

The increase in global fish consumption and the decrease of wild fish stocks are the main reasons behind the continuous development of marine aquaculture (FAO Fisheries Division, 2006, <http://www.fao.org/docrep/009/a0874e/a0874e00.htm>).

The worldwide expansion of the marine fish farms, however, has always been generating concern on the possible impacts for coastal ecosystems. Already in 1995, the Food and Agriculture Organization (FAO) of the United Nations adopted a Code of Conduct for Responsible Fisheries. The Code provided the necessary framework for national and international efforts to ensure sustainable exploitation of aquatic living resources. A particular attention was paid to the aquaculture growth in accord to the sustainable and integrated use of the environment, taking into account the fragility of coastal ecosystems, the finite nature of their natural resources and the needs of coastal communities. In 2001, following the same direction, the European Union started to set up a strategy for a sustainable aquaculture development with the Biodiversity Action Plan for Fisheries (COM (2001) 162) and the European Strategy for Sustainable Development (COM (2001) 264). These two documents led to the more recent and specific Strategy for the Sustainable Development of European Aquaculture (COM (2002) 511).

Marine aquaculture operations are still very expensive and the only mean to sustain profitability is to intensify fish production. Unfortunately this intensification increases the already existing concerns about reaching and getting over the natural capability of the environment. The scientific literature has identified in the release of particulate waste products the main cause of environmental impact due to the presence of marine fish farms (Hall et al., 1990; Holmer & Kristensen, 1992; Karakassis et al., 2000). The particulate wastes increase the organic load on the benthic environment and might determine changes in the community structure and in the biodiversity of the benthic assemblages (Tsutsumi et al., 1991; Wu et al., 1994; Vezzulli et al., 2002, 2003). Therefore we are in need for predictive tools able

to assess earlier whether or not, the establishment of a new farm (or the permission for an increase in production of an already existing one), can result in a potential impact on the surrounding environment.

Numerical models can represent the right tools to perform environmental impacts prediction and to test different scenarios. The interest in tracking aquaculture wastes with mathematical models, in fact, has been rapidly increasing in time (Henderson et al., 2001). In the past we have passed from using analytical models describing over simplistic dispersion patterns in a constant flow in time and space (Gowen et al., 1989), to implementing equations with too many simplifying assumptions about hydrodynamics (Gillibrand & Turrell, 1997). Others have developed particle tracking models using hydrographic data and were therefore limited in their simulations by the sparse data in time and in space (Cromey et al., 2002). Ocean dynamics, instead, are usually very complex and ocean ecosystems are likely to experience current reversals and flow variability. Pioneering numerical studies used circulation models focusing on strongly tidally driven systems. In this case, the flow could have been considered obeying two-dimensional (2D) vertically averaged dynamics (Panchang et al., 1997; Dudley et al., 2000). Unfortunately, the 2D approximation can result inappropriate in more complex and dynamical systems where vertical phenomena affect the dispersion of different particles. Having this in mind, some of us were the first ones to directly take into account the three-dimensional (3D) ocean circulation and its variability in tracking different aquaculture wastes (Doglioli et al., 2004a). Nevertheless, to our knowledge, Doglioli et al. (2004a) (hereinafter referred as DMVT04) still represents the only application of a 3D hydrodynamical model for aquaculture purposes.

The present study takes place following the continuous effort in improving the framework initially set up by DMVT04. The improvements and the assessment of their relative importance are mainly in three directions and represent the core and the original aspect proposed by this work. Namely, in this study (a) we improved

our hydrodynamics using real historic current-meter data to force the simulations;  
(b) we improved our dispersion using a larger number of particles and updating the  
settling velocity values specifically for Mediterranean fish species and for their feed;  
and finally (c) we add a new coupled benthic module to consider the environment  
response to the organic load from the cages.

In DMVT04 some of us used idealized winds to force simulations. The choice  
of the winds was based on a statistical treatment of 34 years of wind data and  
it allowed to carry out a complete 12-day hydrodynamic simulation during which  
wind direction and speed were changing according to a typical local meteorological  
sequence. In a later paper, however, some of us successfully used historical current-  
meter data to study the hydrodynamic characteristics of the area under examination  
(Doglioli et al., 2004b). Since this study effort is toward a more and more realistic  
scenario, we decide to implement the already validated forcing setup used in Doglioli  
et al. (2004b). This mainly implies that the open boundaries conditions and the  
forcing evaluation are improved by applying realistic current measurements.

On the other hand, settling velocity values for uneaten feed and faeces represent  
key parameters for aquaculture waste dispersion models. The lack of values specifi-  
cally targeting Mediterranean fish and their feeds obliged DMVT04 to use the only  
values available in the literature, i.e. the ones measured for salmonids (Chen et al.,  
1999a,b). However, two recent works filled this important gap. On one side, some of  
us, in Vassallo et al. (2006) presented the settling velocities of a feed usually utilized  
in Mediterranean farms (the ‘Marico Seabass and Seabream’ pellets produced by  
Coppens International), while on the other side, Magill et al. (2006) measured the  
settling velocities of Gilthead Sea Bream and Sea Bass faecal particles collected in  
sediment cores in a Greek fish farm. As second original aspect, this study uses these  
new values paying particular attention to the role they play in the overall results.

Finally, we recognize that following only the fate of the particles as we did in  
DMVT04 is not sufficient to correctly assess the organic load on the sea bottom. The

modeling effort should consider the natural capability of the benthic environment in reacting and absorbing fluctuations in the organic load. Our model framework is integrated with an additional new numerical benthic degradative module, the Finite Organic Accumulation Module (FOAM). FOAM is mainly based on the ideas expressed in the work of Findlay & Watling (1997) (hereinafter referred as FW97). They proposed an index of impact based on the ratio between the quantity of oxygen supplied to the sediment and the quantity of oxygen demanded by the sediment. The oxygen supply is calculated through Fickian diffusion and it is in function of the near-bottom flow velocities, while the oxygen demand is based on the organic load from the cages and it is strongly related to the microbial benthic metabolism rate. As pointed out by the same authors, the equations proposed by FW97 can be easily exploited by numerical modelers since the only needed input variables are the bottom flow velocities and the organic flux toward the seabed. Since our model does consider the vertical dimension, it is also able to provide these important required data. Furthermore, its intrinsic Lagrangian nature allows a simple numerical implementation of the ideas proposed in FW97.

The rest of this paper is organized as follows. In Section 2 a description of the study area and the details of the modeling effort are provided. The results of the numerical experiments are presented in Section 3 and discussed in Section 4. Finally the conclusions are given in Section 5.

## 2 Methods

The simulations are carried out for the off-shore fish farm located in the Ligurian Sea already described in DMVT04 (Fig. 1). The sea cages are located at about 1.5 km from the coast and they cover an area of 0.2 km<sup>2</sup>. The bottom depth ranges between 38 m and 41 m. The farm is composed of 8 fish cages with a capability of 2000 m<sup>3</sup> each. The reared biomass is 20 kg m<sup>-3</sup> for an annual mean production of

about 200 ton year<sup>-1</sup>. The fish in the cages are Gilthead Sea Bream (*Sparus aurata*) and Sea Bass (*Dicentrarchus labrax*).

The modeling framework consists of different models which are coupled together into a single functional unit (Fig. 2). The hydrodynamic model is the Princeton Ocean Model (POM) and it is used to derive space and time information of the circulation of the coastal area. POM is coupled online with the three-dimensional Lagrangian Assessment for Marine Pollution Model (LAMP3D). LAMP3D is used to track the particle positions in time and space. The Finite Organic Accumulation Model (FOAM) represents the biochemical component of the modeling system and it uses POM and LAMP3D outputs to estimate the eventual environmental impact due to the organic load from the cages. POM and LAMP3D calculate the bottom velocities and the particle fluxes to the bottom and these values are then used by FOAM to calculate the final organic load in each mesh of its numerical domain.

The following part of this section gives a more detailed description of the whole modeling framework.

## 2.1 The advective and dispersive models: POM and LAMP3D

Some historical measurements of the coastal current in the area are available in terms of current-meter time series and hydrographic surveys, covering a total of 10 months during 1978 - 1979 (Astraldi & Manzella, 1983). Data are archived in the SIAM database (<http://estaxp.santateresa.enea.it/www/siams/prov102.html>), and they have been kindly provided to us by the Italian National Agency for New Technologies, Energy and Environment (ENEA) and the National Research Council (CNR). In this study, we concentrate on the winter-spring period, when the currents are stronger and better defined and the stratification is being formed. We select the period from February 8th 1979 to June 30th 1979 and we force the model on the eastern boundary. At the western boundary a radiation condition is posed. The described setup is the same used and validated in Doglioli et al.

(2004b). The reader is referred to this paper for a more detailed description of the boundary conditions and for their validation. Here, complete four-month simulations are carried out, obtaining current data necessary for the dispersion-degradation runs. The first velocity value ( $U = -0.19 \text{ m s}^{-1}$ ), measured on February 8th 1979, is provided on the whole domain as initial condition for all the simulations. Since the objective of this work is simulating longer time periods, we cyclically repeat the real current-meter data as boundary conditions to force the runs. Consequently, the organic matter accumulation on the seabed can be estimated for longer time and the dependence of the model results on the initial condition reduced.

Moreover, since the primary focus of this study is the organic load on the seafloor and not the fate of the dissolved nutrients, we adopt a new setup respect to the one used in DMVT04 for the hydrodynamical model POM and the dispersive model LAMP3D (see Fig. 1). The POM grid has  $115 \times 80$  meshes with a spatial resolution of 400 m along the  $x$ -direction and 200 m along the  $y$ -direction. The LAMP3D numerical domain, instead, is smaller ( $8 \text{ km} \times 4 \text{ km}$ ), and it is nested in the POM grid with the same spatial resolution ( $400 \text{ m} \times 200 \text{ m}$ ).

The other dispersive parameters are unchanged with respect to DMVT04, with the exception of the Lagrangian particle number that was increased to 620000 for a greater precision and a better rendering. The DMVT04's assumptions on the organic carbon concentration in feed and faecal waste are adopted. In particular, the value of 5% for the feed loss was recently confirmed by results of MERAMED project (<http://www.meramed.com>). Nevertheless, since the number of particles is increased with respect to DMVT04, we calculate new conversion factors for uneaten feed and faecal waste (Table 1). We also keep calculating nitrogen loading rates for validation purposes (see Section 3) using the same conversion factors used in DMVT04 for nitrogen.

The lack of data for Mediterranean species obliged us in DMVT04 to use the values proposed by Chen et al. (1999a) and Chen et al. (1999b) for salmonids. Re-



cently Magill et al. (2006) have measured the settling rates of faecal material of Gilthead Sea Bream and Sea Bass, while, under laboratory conditions reproducing the Mediterranean sea water, Vassallo et al. (2006) have provided the settling velocity values of a typical growing sequence of feed pellets for the same species. We therefore used the values of these recent works in our simulations.

All the parameters used in the hydrodynamic and dispersive models are summarized in the upper part of Table 1, while the different settling velocity values are reported in Table 2.

## 2.2 The benthic module: FOAM

A new bottom boundary condition is implemented in our model. When a numerical particle touches the seabed, it is considered as biodegradable settled matter and it is treated by the benthic module FOAM. FOAM covers the same area of the dispersive model but its resolution is 10 times higher, namely  $40 \text{ m} \times 20 \text{ m}$  (Fig. 1). This is possible because all the FOAM calculations are performed off-line.

According to FW97, the organic accumulation on the bottom leads to different rates of mineralization in relation to the level of stress the seabed is exposed to. In order to simulate the biological reaction of the microbial benthic community to the variations in the organic enrichment, we assign the status of the sediment in each grid mesh according to the ratio between the benthic oxygen supply and the demand.

The oxygen supply is in function of the near bottom velocities and can be calculated by simple Fickian diffusion arguments and expressed by the empirical relation

$$\text{O}_2^{sup} = A + B \cdot \log(\bar{v}) \quad (1)$$

where  $A$  and  $B$  are constants (see Table 1) and  $\bar{v}$  is a time averaged current velocity taken at 1 m from the bottom. It is important to note that  $\bar{v}$  is just the numerical value of the bottom flow velocity when it is expressed in  $\text{cm s}^{-1}$ . In our model

this value is obtained by linear interpolation of the velocity in the deepest vertical grid cell and by using as time interval for the average  $\Delta t = 2$  hours. This choice was already made by FW97 to describe oxygen supply to the benthos. Moreover, this time interval seems to be critical since a 2 hour exposure to reduced oxygen and elevated hydrogen sulfide concentrations causes permanent damage to the gill tissues of sensitive infauna (Theede et al., 1969). The same choice of  $\Delta t = 2$  hours is also supported by the more recent work by Morrissey et al. (2000).

The oxygen demand, instead, is in function of the organic carbon flux toward the sea bottom  $Flx^{Bot}$  according to the relation

$$O_2^{dem} = C \cdot Flx^{Bot} + D \quad (2)$$

where, again,  $C$  and  $D$  are just constants (Table 1). If  $i$  and  $j$  are the grid mesh indexes in the  $x$  and  $y$  directions respectively, the carbon flux  $Flx^{Bot}$  in each grid mesh  $(i, j)$  at the instant  $k$  is calculated on the basis of the number of particles reaching the bottom,  $n_{i,j}^{Bot}$ , during an integration time interval  $dt$ , i.e.

$$Flx_k^{Bot} = \frac{n_{i,j}^{Bot} \cdot w^C}{dt \cdot \Delta x \cdot \Delta y} \quad (3)$$

In the equation (3),  $\Delta x$  and  $\Delta y$  are the horizontal grid sizes while  $w^C$  stands for the adopted organic carbon conversion factor before introduced and listed in Table 1. As already pointed out,  $w^C$  varies if we consider feed or faeces.

Once the model provides  $O_2^{sup}$  and  $O_2^{dem}$  for each grid mesh, we can calculate the index of impact  $I$  as suggested by FW97 as

$$I_{i,j} = \frac{O_2^{sup}}{O_2^{dem}} \quad (4)$$

Based on  $I$  we can identify three different levels of stress: non-stressed sediments, intermediate-stressed sediments and high-stressed sediments. FW97 suggested that when  $I > 1$ , the supply of oxygen is in excess of the demand and therefore the impact is minimal. When  $I \approx 1$  the impact can be moderate while when  $I < 1$ , the sediment exhibits the azoic sediment endpoint and the impact results to be high. In our model the discrete FW97 criterion for the different levels becomes

- 259        · no stress,                if    $I_{i,j} > 1 + \Delta_{fw}$ ;
- 260        · medium stress,        if    $(1 - \Delta_{fw}) \leq I_{i,j} \leq (1 + \Delta_{fw})$ ;
- 261        · high stress,            if    $I_{i,j} < 1 - \Delta_{fw}$ .

262    Sensitivity tests on the  $\Delta_{fw}$  parameter are performed in a range varying from  $\Delta_{fw} =$   
 263    0.05 to  $\Delta_{fw} = 0.5$ . We observe no meaningful differences, so, for precautionary  
 264    reasons, the value of  $\Delta_{fw} = 0.5$  is adopted.

265        When the level of stress is decided according to the value  $I_{i,j}$ , different rates of  
 266    mineralization are used in each grid mesh. Practically in our code, this is obtained  
 267    subtracting different quantities to the already calculated organic carbon concen-  
 268    tration fluxes. The subtracted amounts are the same of FW97 and are shown in  
 269    the lower part of Table 1. On the basis of the obtained fluxes, the organic carbon  
 270    concentration  $Conc^{Bot}$  in each grid mesh  $(i, j)$  is calculated as

$$271 \qquad \qquad \qquad Conc^{Bot} = \sum_{k=1}^{NT} Flux_k^{Bot} \cdot dt \qquad (5)$$

272    where  $NT$  is the number of the time intervals of the simulation.

273        All the parameters used in the benthic module are summarized in the lower part  
 274    of Table 1.

## 275    3    Results

276    The modeled water circulation is in agreement with the past literature in the area:  
 277    the simulations show the presence of the observed westward transport (Astraldi &  
 278    Manzella, 1983; Astraldi et al., 1990), persisting for almost all the simulated period  
 279    (winter-spring). The obtained general circulation also agrees with other numerical  
 280    experiments such as Baldi et al. (1997) and DMVT04. It is also possible to observe  
 281    current separation and eddy formation behind the Portofino Promontory like in  
 282    Doglioli et al. (2004b). For a more quantitative hydrodynamic validation, we use the

same approach as in DMVT04. Current data simulated by the model are compared  
 with data collected by one current meter, C1, located at 2 km on the west of the farm.  
 Current speed and direction were sampled every hour at 20-m depth from February  
 1993 to March 1994. Table 3 shows current data from C1 and the model outputs.  
 When we use only one cycle at the eastern boundary and we prescribe the first  
 velocity value on the whole domain as initial condition, the seasonal averages from  
 the observations are systematically lower than the model ones (see values for the first  
 cycle). When we cyclically repeat the boundary conditions to force the runs and we  
 use as initial condition the last velocity field of the previous cycle, the comparison  
 with the C1 data improves (see values for the fifth cycle). We speculate that the  
 larger discrepancy observed in the first cycle is due to the artificial highly energetic  
 initial condition. Therefore, we decide to run five cycles of linked simulations and  
 we subsequently neglect the first two in order to reduce the sensitivity to the initial  
 conditions. The three linked cycles account for a total of 430 simulated days and  
 their averages are also proposed in Tab. 3. In this case, data are very close to the  
 values calculated by the model. Current direction agrees with the observed along-  
 shore water movement. Sporadic current reversals are also simulated thanks to the  
 inversions of the direction of the velocity at the inflow boundary condition.

At the same time, we can use sediment observations around the cages to validate  
 our dispersive runs. A Van Veen grab was used to collect sediment samples in three  
 repetitions in each of the four stations surrounding the fish farm (see DMVT04,  
 Fig.7). Respect to DMVT04 additional recent data were collected in the same  
 stations. All the samples were analyzed for total nitrogen and total phosphorus.  
 The comparison between absolute values of these data and the model outputs is not  
 possible since, in order to express both of them in the same units, we need heavy  
 assumptions on the sediment density as well as on the sampling methodology. We  
 therefore use the same approach used in DMVT04. Fig. 3 shows the agreement  
 between field and modeled data. In particular, field sediment nutrients are highest

in station S2 and lowest in station S4, which agrees with model output for total nitrogen under westward transport. To facilitate the reader, in the same Fig. 3, we also show the performance of the old setup adopted in DMVT04 and the field data as they were at that time.

The above comparison with the only data available in the area, allows us to focus on the dispersion model and on the benthic modeled impact. The time series of the dispersion model output are also referred to the three last cycles of linked simulations. In order to explore the differences in the runs varying waste typology, release condition and settling velocity, we set up the following experiments:

A1) slowly sinking feed in continuous release;

A2) quickly sinking feed in continuous release;

B1) slowly sinking feed in periodical release;

B2) quickly sinking feed in periodical release;

C1) slowly sinking faeces (continuous release);

C2) quickly sinking faeces (continuous release).

Note that for periodical release we mean that the feed is supplied twice a day, and slowly and quickly sinking are referred to the minimum and maximum values listed in Table 2 for the two different waste typologies. In Table 2 the slowly values are indicated with a single arrow pointing toward the bottom ( $\downarrow$ ), while the quickly values with a double one ( $\Downarrow$ ).

Results from the benthic module are presented in relation to (i) the extension of the impacted area, (ii) the position of this area in terms of its barycenter, (iii) the benthic trophic conditions and (iv) the predicted organic concentration at the barycenter. The choice of these parameters allows to simply and objectively estimate respectively the degree and the location of the eventual impact.

The impacted surface  $S$  is the sum of the areas of the grid meshes where particles are still present even after the benthic degradation activity. The position of the barycenter  $(x_b, y_b)$  of this area is basically a position weighted by the number of particles left in each cell after the degradation. It is simply expressed as

$$x_b = \frac{\sum_{j=1}^N \sum_{i=1}^M i \cdot n_{i,j}^{left}}{n_{Tot}^{left}} \quad (6)$$

$$y_b = \frac{\sum_{j=1}^N \sum_{i=1}^M j \cdot n_{i,j}^{left}}{n_{Tot}^{left}} \quad (7)$$

where  $M$  and  $N$  are the numbers of meshes in the  $x$  and  $y$  directions,  $n_{i,j}^{left}$  is the number of particles left on the bottom in the mesh  $(i, j)$  and  $n_{Tot}^{left} = \sum_{j=1}^N \sum_{i=1}^M n_{i,j}^{left}$  is the total number of particles left on the bottom after the degradation. The benthic trophic condition and the predicted organic concentration at the barycenter are simply given by the parameter  $I$  and  $Conc^{Bot}$  in the grid mesh corresponding to the barycenter position.

We initially describe the effects on the extension of the impacted area. Fig. 4 shows the time series of the calculated extensions in the different experiments and the temporal variations of the modeled current velocity near the cages (Fig. 4D). The slowly sinking feed particles continuously released (Fig. 4A, solid black line) are dispersed by the current a little bit more than the quickly sinking ones (dashed gray line). This is also confirmed by the time averages and the standard deviations for the experiments A1 and A2 (see Table 4). The situation changes when we consider periodical release (Fig. 4B). In this case both slowly and quickly sinking particles are dispersed on a larger area than in the continuous case. However, while for slowly particles this area is much larger and less variable in time than in the continuous release, for quickly ones, the area is just a little bit bigger and more variable (see Table 4). The variability of the dispersion is therefore associated with the current velocity and it increases both with periodical release and with decreasing settling velocity values. For faecal pellets (Fig. 4C), the impacted area is smaller than in

the previous cases. Moreover, faecal wastes show a much greater time variability than the uneaten feed, no matter what the feed release is. The slowly sinking faecal particles impact a smaller areas respect to the quickly ones and also the variability is smaller than the quickly sinking ones (Table 4).

Fig. 5 better visualizes what stated so far and, at the same time, it shows the position of the barycenter of the impacted area. In this plan view, we schematize the extension of the impacted area with a circle centered in the barycenter and having an equivalent area to the one already calculated. The gray scale represents the time evolution of the results every sixty days, while a circle is drawn every ten days. In the case of feed, for both continuous and periodical releases, the barycenter of the impacted area is found at approximately 25 m southwestward from cages. For the same simulations not such a significant time variability is observed (Fig. 5A1, A2, B1 and B2) and this means that the impacted area is always larger and that higher stressed levels are expected. In the case of faecal wastes, instead, the barycenter shows a great time variability, according to changes in current direction and intensity (Fig. 5C1 and C2). This variability results in a dispersion of the faecal particles in different areas and therefore lower stressed levels are expected.

To better emphasize these results, we can look at the scatter diagram of the parameter  $I$  at the barycenter position in time (Fig. 6). For clarity, all values greater than 2 are artificially assigned to 2 in this figure. For feed particles continuously released (Fig. 6A),  $I$  mainly stays in the no-stressed range (i.e.  $I > 1.5$ ), sometimes goes up to the intermediate-stressed range, but the high-stressed level is rarely reached. There is a slight tendency for quickly particles to stay more in the intermediate regime than the slowly ones (Table 4). For periodical release (Fig. 6B),  $I$  is often in the no-stressed range, very rarely in the intermediate-stressed range but it reaches the high-stressed level more frequently than before. An easy and quick check shows that the high-stressed values are registered, in this case, in the period going from 2 to 4 hours after the release. No significant differences can be observed

between slowly and quickly sinking particles. For faecal wastes (Fig. 6C), the parameter  $I$  is practically always greater than 2 (for this reason in the plot all dots are squeezed on the top) for both slowly and quickly sinking particles.

Finally, the mean values of the computed organic matter concentration  $Conc^{Bot}$  remaining on the seabed at the barycenter position after the degradation are reported in the last column of Table 4. The organic carbon amount due to feed waste almost linearly increases with time and the maximum values are reached in the case of fastest feed particles in periodical release. The faecal waste instead seems to be completely degraded and it does not contribute to organic carbon concentration at the bottom.

All the results are summarized in Table 4.

## 4 Discussion

As regards both hydrodynamics and dispersion the new model setup presented here shows a remarkable improvement with respect DMVT. In particular, the inflow forcing based on historic current-meter data and the linking of simulations allow a more realistic modeling of the study area circulation. This fact represents a key result because the current direction and intensity strongly influence the position of the impacted area and the settled matter degradation, as remarked in Morrissey et al. (2000) and FW97. Nevertheless these processes are strongly non linear and it is difficult to schematize the role played by each model parameter.

When settling velocity of particles is not too slow (one order of magnitude less than the current velocity, as a lower limit) the impacted area does not vary and the barycenter position depends on the main direction of the current. For very slow settling particles instead the variability of the current starts to play a major role. For this reason, the uneaten feed barycenter remains practically motionless and, on the contrary, the faeces barycenter is very mobile.



At the same time the current intensity affects degradation of particles in two ways. On one hand, a strong current makes degradation more efficient bringing a greater oxygen quantity to the sediment. On the other hand, the same strong current increases the waste dispersion producing a wider impacted area on the bottom, but also a lesser waste concentration. In these conditions a greater degradation can happen. The latter situation is always observed in our results for faeces. For feed instead the strong settling velocity generates great stores that are not removed also if strong current happens. Probably also this fact supports the observed stability of the impact area size and position.

The fact that we used settling velocity values from Magill et al. (2006) calls for a comparison with their results. To do this, we calculated in the impacted area barycenter the accumulation rates of 11 g faeces  $\text{m}^{-2} \text{year}^{-1}$  and 19 g faeces  $\text{m}^{-2} \text{year}^{-1}$  for slowly and quickly sinking particles, respectively. These values are about 2 orders of magnitude smaller than the Magill et al. (2006)'s ones. Nevertheless two explanations could be given. First, in Magill et al. (2006) the total biomass of fishes is not reported, keeping us from a right quantitative comparing. The policy of the studied fish-farm is to keep low biomass per cage (Roberto Co', AQUA s.r.l., personal communication), then it is high probable that Greek fish farm studied by Magill et al. (2006) has higher biomass per cage. Second, with FOAM module we introduced the degradation of the settling organic carbon, not considered instead by Magill et al. (2006). Nevertheless, we adopted the degradation rates proposed by FW97 for Atlantic fish farm that can be too high with respect the Mediterranean ones. Moreover, to consider degradation of faeces by oneself can implies an overestimation of the degradation. On the other hand, according to Magill et al. (2006) we found a greater impact near the cages due to the faeces of *D. Labrax* than *S. Aurata*'s ones.

In our results the uneaten feed are confirmed to be the primary cause of ecological impact on the benthos community, according to Beveridge et al. (1991), Vezzulli

et al. (2003). Actually, the organic carbon content into the feed is higher than into the faeces, but also the faeces are more degraded, as noted above. This fact motivated us to study in more detail the feed release conditions. We found that the twice-in-a-day release generates i) more frequent conditions of high stressed sediments and ii) larger impacted areas than a continuous release. These results support the use of self-feeders that are already proposed by several authors in order to reduce the uneaten feed losses with no effect on growth rates (Azzaydi et al., 1998, and references therein).

## 5 Conclusions

Since the aquaculture is the foodstuffs production activity with the most rapid growth in the world, and in particular marine fish farmed in intensive system, it is necessary to develop tools to predict their environmental impact.

In this study we improved the capability of the POM-LAMP3D model (DMVT04) developing both a more realistic advection-dispersion setup and a new benthic module, named FOAM (Finite Organic Accumulation Module). FOAM values the benthic degradation of organic carbon considering three different levels of the sediment stress, following FW97's empirical model. We performed several runs to simulate different scenarios varying waste typology (faecal or feed), settling velocity of particles (on the basis of feed dimensions, fish size and reared species) and release conditions of feed (periodical or continuous).

We obtained more satisfactory results for the hydrodynamics and dispersion in the study area with respect DMVT04. Then we focused our attention to benthic modeled impact. FOAM module revealed its ability to simulate different scenarios switching suitable parameters.

The results presented in relation to extension of impacted area and position of its barycenter, show that the continuously released feed are forced to settle in a narrow

area near the cages (impact area maximum 6500 m<sup>2</sup>; barycenter shifting amplitude 10 m; cages maximum distance 25 m) while twice-in-a-day released feed take up a larger area centered near the cages (maximum area 8500 m<sup>2</sup>; barycenter shifting amplitude 15 m; cages maximum distance 25 m). The faecal pellets are accumulated on a smaller area within a greater and more variable range from the cages (maximum area 4000 m<sup>2</sup>; barycenter shifting amplitude 100 m; cages maximum distance more than 50 m) with respect to the uneaten feed. The maximum impacts, in terms of both stress parameter  $I$  and organic carbon concentration, are due to the quickly settling feed, released in periodical mode and during slow current periods. Some mitigation of the impact is observed if feed is continuously released. Then, the use of self-feeders has been suggested to the farmers. On the other hand, further investigations are probably necessary to verify the impact of combined feed and faeces settling. At this purpose mineralization rates for Mediterranean conditions and validation with specific in-situ measurements are required.

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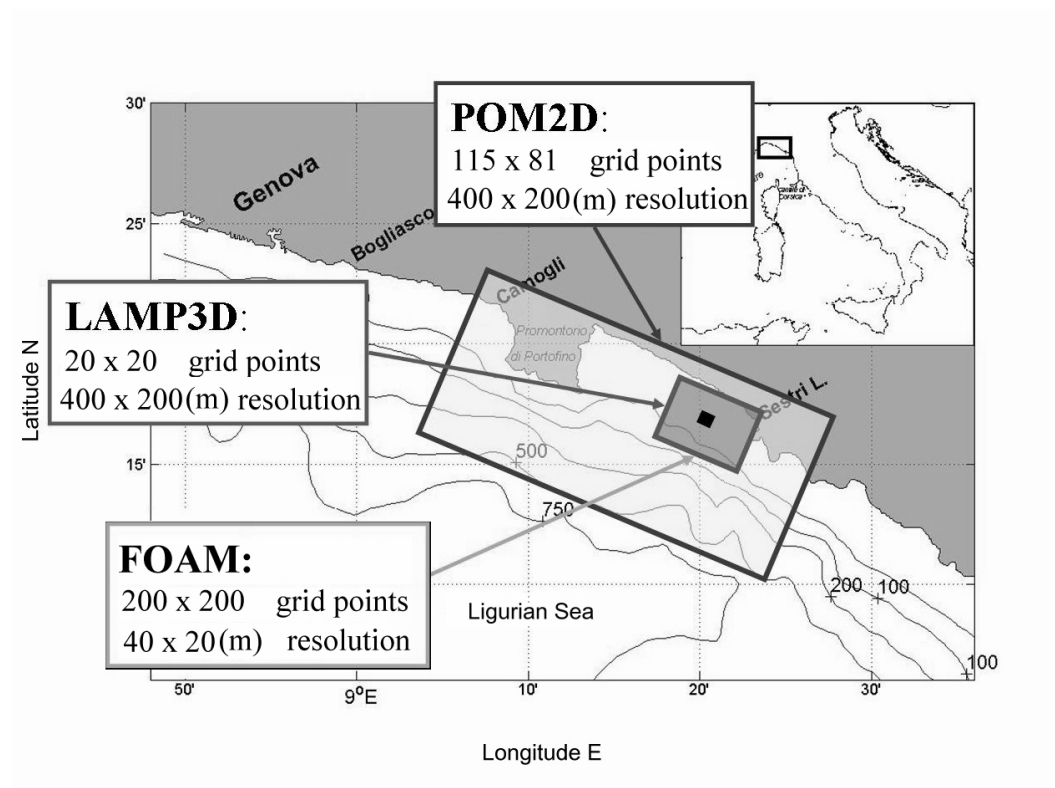


Figure 1:

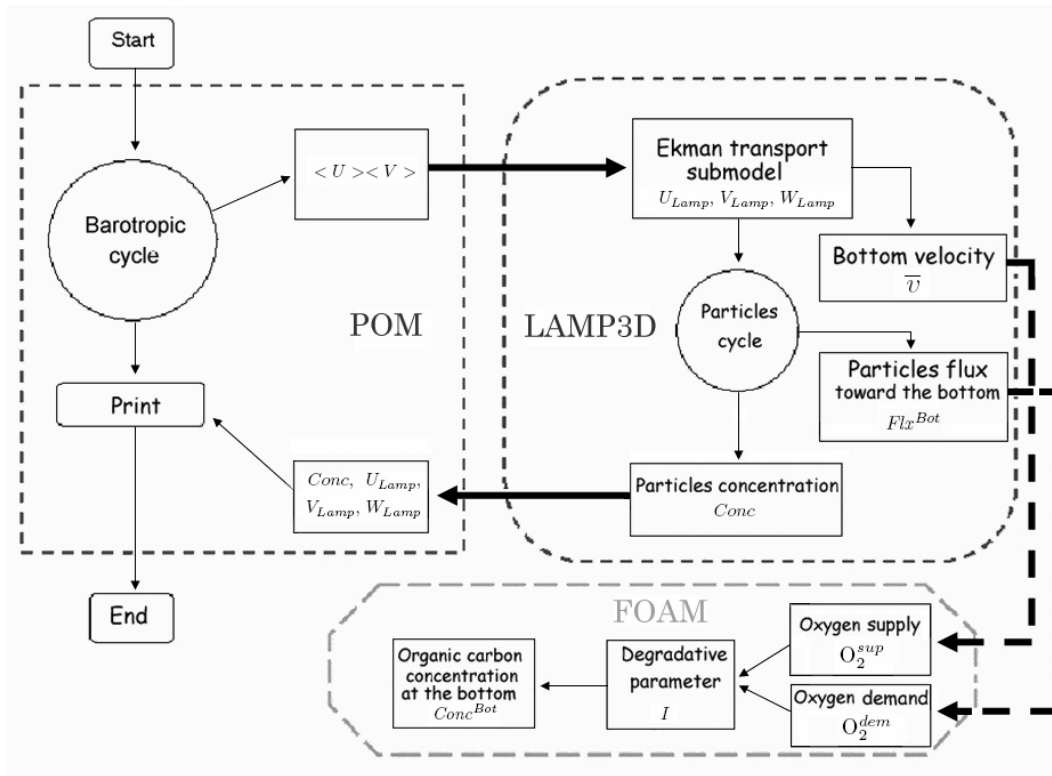


Figure 2:

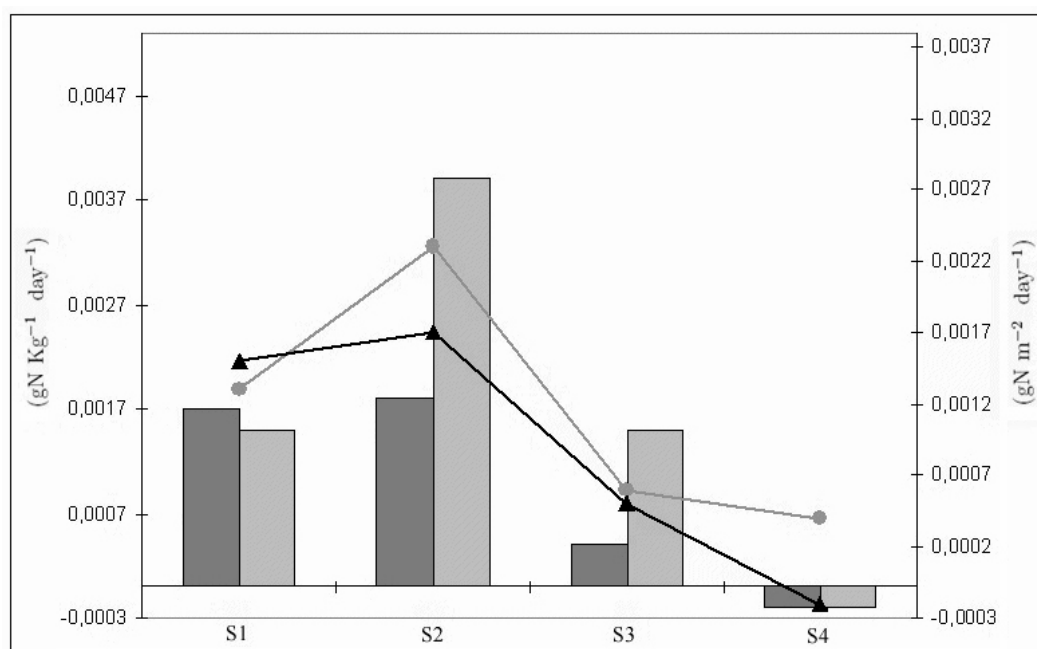


Figure 3:

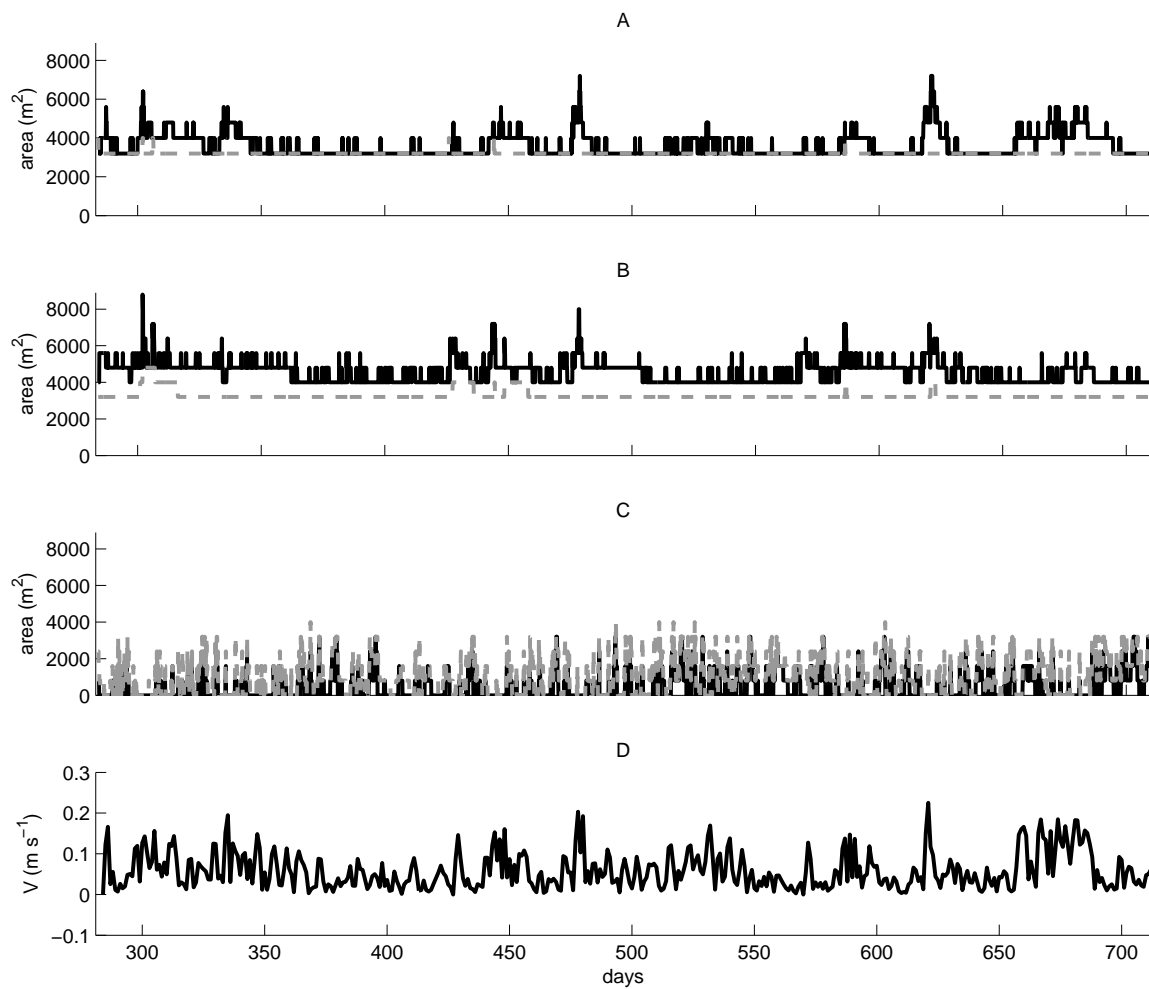


Figure 4:

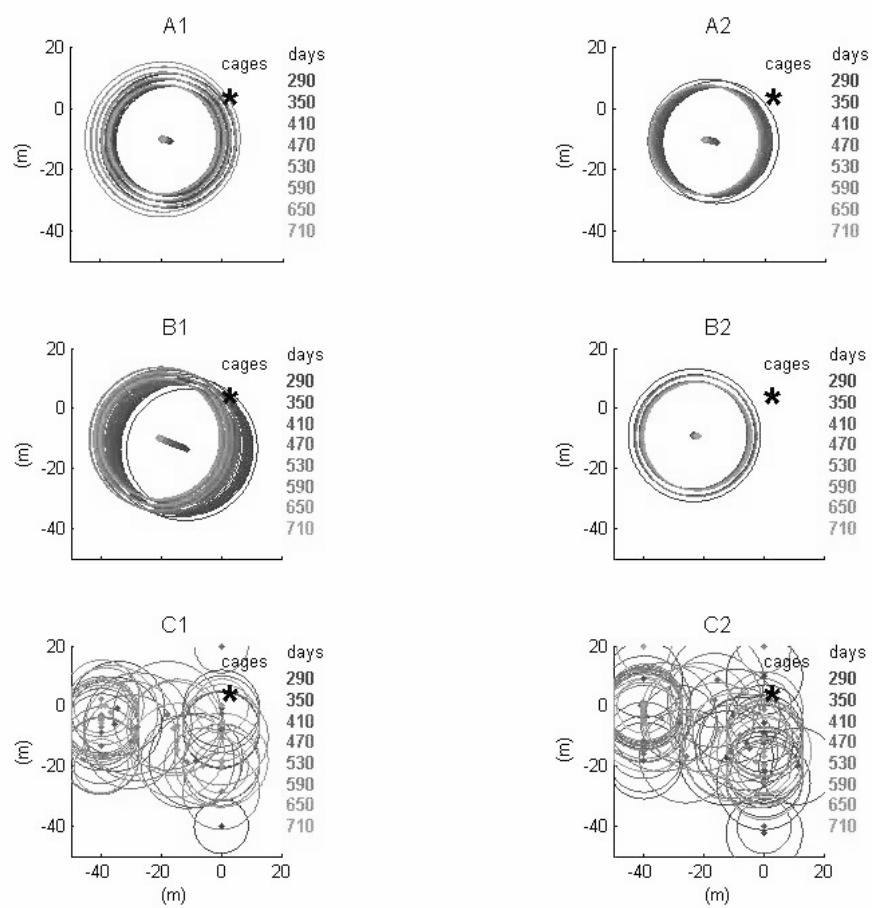


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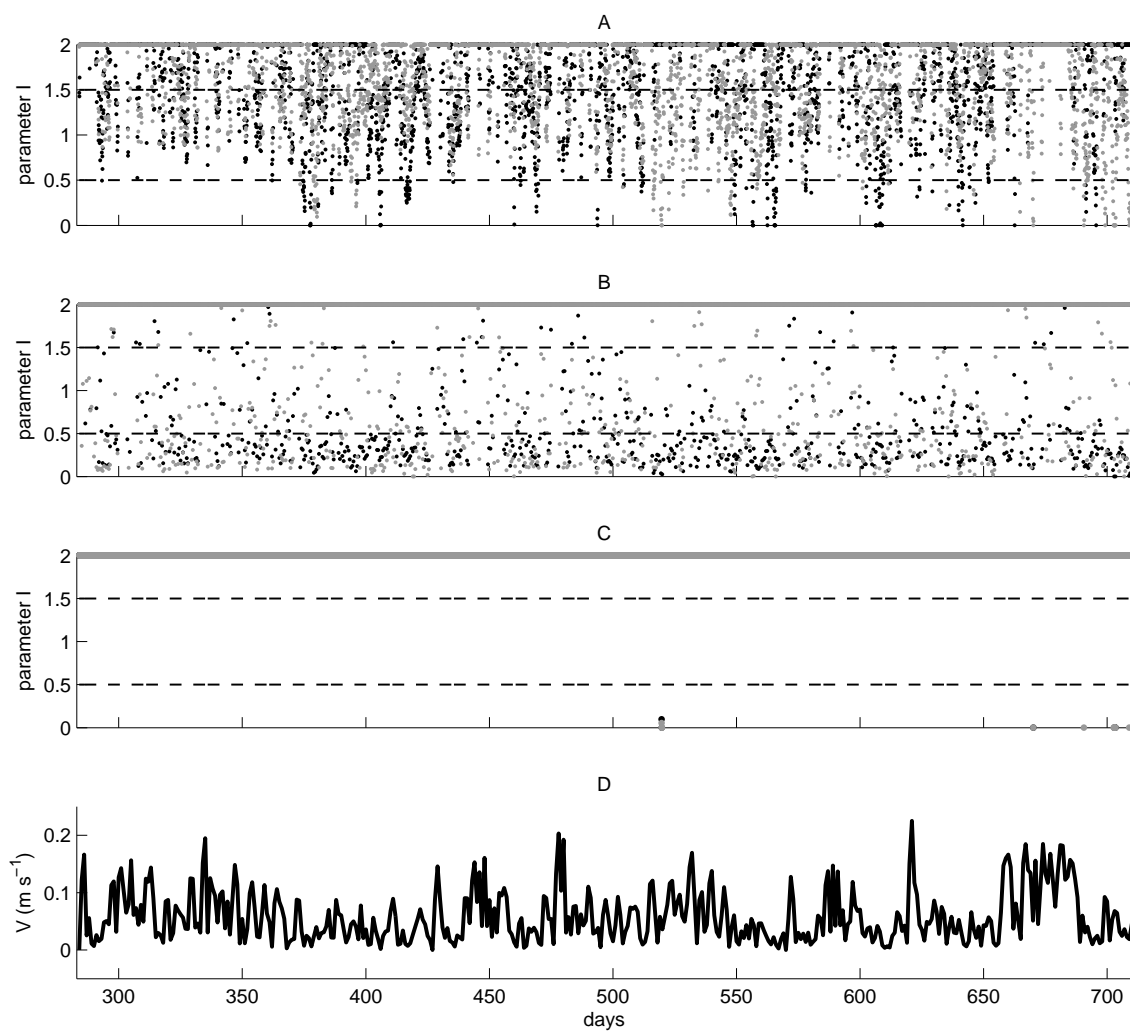


Figure 6:

POM-LAMP3D parameter	value
POM physical domain (km)	46x16
LAMP3D physical domain (km)	8x4
Horizontal resolution (m)	400x200
Vertical resolution (m)	10
Barotropic cycle time step (s)	1
Smagorinsky diffusivity coefficient	0.1
Asselin filter coefficient	0.05
Ekman depth $\delta_E$ (m)	50
Wind drag coefficient $C_d$	0.001
Horizontal standard deviation $\sigma$ (m)	3.46
Particle cycle time step (s)	60
Number of particles	620000
Feed conversion factor for organic carbon $w_{feed}^C$ (mmolC particle <sup>-1</sup> )	308.6
Faeces conversion factor for organic carbon $w_{faeces}^C$ (mmolC particle <sup>-1</sup> )	5.8
Feed conversion factor for nitrogen $w_{feed}^N$ (mmolN particle <sup>-1</sup> )	167.8
Faeces conversion factor for nitrogen $w_{faeces}^N$ (mmolN particle <sup>-1</sup> )	66.4
FOAM parameters	value
Physical domain (km)	8x4
Horizontal resolution (m)	40x20
$O_2$ supply parameter $A$ (mmolO <sub>2</sub> m <sup>-2</sup> d <sup>-1</sup> )	736.3
$O_2$ supply parameter $B$ (mmolO <sub>2</sub> s m <sup>-3</sup> d <sup>-1</sup> )	672.5
$O_2$ demand parameter $C$ (mmolO <sub>2</sub> mmolC <sup>-1</sup> )	1.07
$O_2$ demand parameter $D$ (mmolO <sub>2</sub> m <sup>-2</sup> d <sup>-1</sup> )	-32.6
Settled matter non-stress $N_s$ (mmolC m <sup>-2</sup> d <sup>-1</sup> )	27.53
Settled matter intermediate-stress $I_s$ (mmolC m <sup>-2</sup> d <sup>-1</sup> )	57.50
Settled matter hyper-stress $H_s$ (mmolC m <sup>-2</sup> d <sup>-1</sup> )	30.59
$I$ range amplitude parameter $\Delta_{fw}$	0.5

Table 1:



Feed pellets		Faecal pellets	
Diameter (mm)	$V_{sed}$ (m s <sup>-1</sup> )	Fish species [size (g)]	$V_{sed}$ (m s <sup>-1</sup> )
3	0.087 ↓	<i>S. Aurata</i> [380]	0.004 ↓
3.5	0.118	<i>S. Aurata</i> [60]	0.005
4.5	0.103	<i>D. Labrax</i> [280]	0.006
5	0.144 ↓	<i>D. Labrax</i> [80]	0.007 ↓
6	0.088		

Table 2:

Observations ( $\text{m s}^{-1}$ )					
	Winter average (std)	Spring average (std)	Summer average (std)	Autumn average (std)	Annual average (std)
C1	0.066 (0.057)	0.075 (0.065)	0.063 (0.052)	0.070 (0.052)	0.069 (0.057)
Model Output ( $\text{m s}^{-1}$ )					
	Winter average (std)	Spring average (std)	Summer average (std)	Autumn average (std)	Overall average (std)
1st cycle	0.076 (0.051)	0.103 (0.084)	- -	- -	0.088 (0.047)
5th cycle	0.059 (0.034)	0.082 (0.066)	- -	- -	0.057 (0.034)
3th $\rightarrow$ 5th cycles	0.064 (0.042)	0.078 (0.050)	- -	- -	0.061 (0.034)

Table 3:

Exp.	Simulation typology (release)	<i>S</i> Impacted area mean $\pm$ std ( m <sup>2</sup> )	Parameter <i>I</i>			Organic concentration mean $\pm$ std ( gC m <sup>-2</sup> )
			no stress (% days)	medium stress (% days)	high stress (% days)	
A1	Slow feed (continuous)	3576 $\pm$ 582	74	22	4	1450 $\pm$ 404
A2	Quick feed (continuous)	3202 $\pm$ 41	71	27	2	1490 $\pm$ 453
B1	Slow feed (periodical)	4513 $\pm$ 563	87	4	9	895 $\pm$ 380
B2	Quick feed (periodical)	3277 $\pm$ 266	88	4	8	1590 $\pm$ 387
C1	Slow faeces	377 $\pm$ 656	99	0	1	< 1
C2	Quick faeces	941 $\pm$ 962	99	0	1	< 1

Table 4: